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Effects of Nano-sized Titanium Powder on the Anti-corrosion Property of Epoxy Coatings on Steel

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The protective performance of epoxy asphalt coatings modified by 200 meshes titanium powder, in mass fractions 2 %, 5 %, 10 %, and 20 %, and coatings without titanium and with mass fractions of nano-sized titanium powder 5 %, 10 %, and 20 %, was studied using electrochemical impedance spectroscopy (EIS) and salt spray test. Moreover, infrared spectrum and X-ray photoelectron spectroscopy (XPS) were used to study the structure of the coatings.

The results show that nanometer titanium may be involved in the reaction solidification process of the coatings. Therefore, the addition of titanium nano-powder to the coatings does not significantly change the physical properties of the coatings (toughness). On the other hand, coatings with nano-sized titanium powder have better protection performance than coatings containing micrometre-sized titanium powder. At the same time, because a chemical key exists between nano-sized titanium particles and the coating agent, the increase in the number of charge carriers in the coating due to the existence of the titanium metal is lower. For this reason, the resistance change order is different from the change law of the coating modified with the micrometre-sized titanium powder, and the change rule of the electrical resistance for the coatings modified by nano-powder titanium cannot be explained by the change of dielectric constants.

Key words: Anti-corrosion property, nano-sized titanium, epoxy coal tar coating

Introduction

Because of the existence of corrosion media such as chlorine, serious corrosion attacks ships, offshore and marine structure. Scholars worldwide have been long committed to the research of marine corrosion and development of anticorrosion agents, and have achieved remarkable results. But so far, the conventional ocean coating inevitably makes microholes or microcracks between the additive and adhesive due to the physical or van der Waals force interactions between the packing and the binder, which provides a channel used to help the corrosion media reach the surface of the protected metal. Therefore, the corrosion resistance of common coating is reduced.

Throughout the history of the development of nano-composite coating, due to the full use of the nano-sized powder, significant changes have taken place in the paint industry. As titanium is the most corrosion-resistant metal in the marine environment, if nano-sized titanium powder is added as packing material to the anti-corrosion coatings, will it have the same effect as micrometre-grade titanium powder? This paper focuses on the previous study of anti-corrosion properties of coatings modified with 200 mesh titanium powder and nano-sized titanium particles.^{3,4}

Experimental

Preparation of samples

Test specimens were coated UNS G10190 panels. The coating was a commercially available epoxy resin (E20) modified with coal tar. As a curing agent, polyamine (650#) was used. Powdered titanium (200 mesh) was added to the coating at room temperature in mass fractions 2 % (numbers T1), 5 % (numbers T2), 10 % (numbers T3), 20 % (numbers T4), and the nano-sized titanium powder (50 – 120 nm) mass fraction was 0 (numbers 0 % nano), 5 % (numbers 5 % nano), 10 % (numbers 10 % nano), 20 % (numbers 20 % nano) respectively.^{3,4}

The panels were cleaned with analytical grade ethanol to remove water and degreased with analytical grade acetone before coating. After stirring thoroughly, the coating was applied to the metal by a model XB-120 coater made by Shanghai Xiandai Environment Engineering Technique Co. Ltd. Curing was carried out at room temperature and, after solidification, the specimens were kept in a desiccator for one week before being tested.

Salt spray test

According to ASTM B117,⁵ the corrosion resistance of samples prepared as described above was tested by the salt spray test for 2000 h.

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EIS inspections

The experimental apparatus for the EIS investigation consisted of a Perspex[®] cylinder attached to the surface of the coated panel via an O-ring made of rubber in order to create a vessel to hold the electrolyte.⁶ The coated panel was the working electrode of electrolytic cell. A saturated Ag/AgCl electrode was used as reference electrode and a platinum foil was used as counter electrode. All EIS experiments were performed at room temperature in aqueous solution with w = 3.5 % of sodium chloride prepared by dissolving analytical grade sodium chloride in distilled water. Experimental tests were carried out by using an EG&G model 273 Potentiostat/Galvanostat connected to a model 5210 Lock in Amplifier and controlled by a computer. Usually, five points were measured for each decade of frequency ranging from 10^5 Hz to 10^{-2} Hz. The amplitude of the superimposed potential was 20 mV. EIS measurements were carried out after 0.5 h firstly, and then once a day. After the EIS experiments, data were analysed by using Zview software.

X-ray photoelectron spectroscopy (XPS) inspection

XPS testing of the coating of UNS G10190 steel was performed by using the source of magnesium.

Results and discussion

The salt spray test results of coatings modified by 200 meshes titanium powder in mass fractions 2 % (T1), 5 % (T2), 10 % (T3), 20 % (T4), and coatings modified by nano-titanium powder (50 – 120 nm) in mass fractions 0 (0 % nano), 5 % (5 % nano), 10 % (10 % nano), 20 % (20 % nano), are shown in Table 1. Clearly visible is the displacement of evenly small bubbles and emerged rust on the coating unmodified with titanium powder, indicating that the coating has been broken down and the steel matrix has been corroded at the point of emerged rust. On the other hand, there are cracks on the coatings modified with 200 mesh titanium. The coatings are more brittle than those without titanium. Therefore, the protective property is low. However, compared with the coatings mentioned above, there is no cracking but only local blistering appeared on the coatings modified with nano-sized titanium powder (50 - 120 nm) in mass fractions 5 % (5 % nano), 10 % (10 % nano), and 20 % (20 % nano). Consequently, the property of the coatings with nano-sized titanium powder is better than that of coating without titanium. The reason is that after adding nano-sized titanium powders, labyrinthic effects are enhanced because of the dispersion and distribution of nano-particles. On the other hand, there probably is some bonding between titanium nano-particles and epoxy modified by coal tar in the process of solidification. Therefore, the defects caused by titanium particles are decreased and the barrier property is promoted.

Table	1	- Results of coatings after 2300 hours of salt spra	y
		testing	

Tablica 1 – Svojstva laka nakon 2300 sati ispitivanja raspršivanjem soli

	,		
Specimen Uzorak	Blistering Mjehuranje	Rust Hrđa	Cracking Pucanje
0 % nano-1	_	even podjednako	-
0 % nano-2	evenly small blisters podjednaki mali mjehuri	some ponegdje	_
0 % nano-3	evenly small podjednaki mali	some ponegdje	-
5 % nano-1	evenly small podjednaki mali	_	—
5 % nano-2	even podjednaki	_	-
5 % nano-3	even podjednaki	—	-
10 % nano-1	locally small lokalni mali	—	-
10 % nano-2	locally small lokalni mali	—	-
10 % nano-3	large blister and stainless metal substrate veliki mjehur, netaknuta podloga	_	_
20 % nano-1	large blister veliki mjehur	some ponegdje	-
20 % nano-2	local lokalno	_	_
20 % nano-3	local lokalno	—	—
T1-1	even, large podjednaki, veliki	_	-
T1-2	even, small podjednaki, mali	-	local lokalno
T1-3	locally small lokalni mali	_	_
T2-1	evenly, small podjednaki, mali	_	—
T2-2	even, small, some large podjednako, mali, neki veliki	_	-
T2-3	even, small, some large podjednako, mali, neki veliki	_	-
T3-1	local lokalno	_	local lokalno
T3-2	evenly, small, some large podjednako, mali, neki veliki	_	-
Т3-3	local lokalno	—	local lokalno
T4-1	local, small, some large lokalno, mali, neki veliki	—	—
T4-2	_	_	local lokalno
T4-3	locally small Iokalni mali	_	local lokalno

T a b l e 2 – Electrical resistance of coatings modified with micro-powder Ti after different immersion times T a b l i c a 2 – Električni otpor lakova modificiranih mikroprahom titanija nakon različitog vremena uranjanja

Immersion time	Electrical resistance/ Ω Električni otpor/ Ω			
vrijeme uranjanja	T1	Τ2	Т3	T4
0.5 hour / 0,5 sati	1.0529 · 10 ¹⁰	$5.8333 \cdot 10^{9}$	$2.122 \cdot 10^{9}$	$1.976 \cdot 10^{9}$
192 hours / 192 sata	$2.6809 \cdot 10^8$	$6.5716 \cdot 10^{8}$	$9.7513 \cdot 10^{8}$	$1.9618 \cdot 10^{9}$

Immersion time	Electrical resistance / Ω Električni otpor / Ω			
Vrijeme uranjanja	0 % nano	5 % nano	10 % nano	20 % nano
0.5 hour / 0,5 sati	$4.98 \cdot 10^{7}$	$6.212 \cdot 10^{8}$	$1.078 \cdot 10^{10}$	$1.159 \cdot 10^{10}$
240 days / 240 dana	$1.161 \cdot 10^{8}$	$4.3041 \cdot 10^{7}$	$6.327 \cdot 10^{8}$	$7.9014 \cdot 10^{7}$

T a b l e 3 – Electrical resistance of coatings modified with Ti nano-powder after different immersion times T a b l i c a 3 – Električni otpor lakova modificiranih nanoprahom titanija nakon različitog vremena uranjanja

The EIS results indicated that within the scope of the study, the epoxy coal tar pitch coating modified with micro-powder Ti immersed in aqueous 3.5 % sodium chloride solution, the resistance of coatings decreased with the increase in Ti content. Moreover, with prolonged immersion time, the order of electrical resistance changed. The resistance of coatings immersed for 192 hours increased with time.³ The EIS data for coatings immersed for different times are shown in Table 2.

However, by analysing the performance of coating with titanium nano-powder, it can be found that if immersed for half an hour, there is no regularity between the resistance of the coating and nano-sized titanium content. The electrical resistance of coating with 10 % nano-sized Ti is similar to that of coating modified with 20 % nano-sized titanium, and the coating without titanium has the minimum.⁴ Whereas, after a long immersion time when the resistance of the coatings is stable, the resistance of coating with 10 % nano-sized titanium powder reaches the maximum, the order of electrical resistance of coating containing nano-powder titanium is different from that of coating containing 200 meshes titanium.

The results indicate that there is a difference between the order of electrical resistance versus nano-sized Ti and 200 meshes titanium content.

It is well known that the number of charge carriers in metal is far greater than that in organic coatings. As a result, because of the addition of the metal powder to organic coatings, the number of charge carriers in the coating containing metal powder should be increased. Moreover, the higher the amount of metal powder in the coating, the greater is the number of carriers.

Therefore, there is probably some chemical bonding during solidification, which makes the decreasing tendency caused by the increase in the number of charge carriers lower, and as a result of which the electrical resistance of coatings containing nano-titanium powder does not decrease with increased nano-titanium content.

In order to verify this view, the coating without titanium and coatings containing 10 % nano-sized titanium powder were tested using XPS. From Fig. 1 it can be seen that the peak of O^{1s} changed from 532.293 eV (without Ti) to 532.719 eV (for coating with 10 % nano-sized Ti). Thus, it could be concluded that the mode of existence of oxygen in the coating had changed because of the addition of nano-sized titanium powder.

The infrared spectroscopy (IR) of unmodified coating and coating modified by 10 % nano-sized titanium powder indi-





Slika 1 – (a) XPS epoksidnog laka modificiranog katranom kamenog ugljena; (b) – XPS XPS epoksidnog laka, modificiranog katranom kamenog ugljena, s 10 % nanočestica titanija

cated that a fine distinction appeared at the low wave numbers and high wave numbers (Fig. 2). The peak of 551.30 cm⁻¹ for coating without nano-sized titanium appears at wave number 556.27 cm⁻¹ for coating with 10 % nano-sized Ti powder. According to references,^{7,8} there are peaks of Ti–O at 638 cm⁻¹, 598 cm⁻¹and 558 cm⁻¹. The offset of the peak at 551.30 cm⁻¹ may be caused by Ti–O bonding, while the bond Ti–O might have been formed during the solidification.



Fig. 2 – Infrared spectrum of the coal tar modified epoxy coatings without titanium and with 2 % nano-sized titanium

S I i k a 2 – Infracrveni spektar epoksidnog laka, modificiranog katranom kamenog ugljena, bez dodataka i s 2 % nanočestica titanija

Based on the analysis mentioned above, the curing reaction of coatings modified by nano-sized titanium is deduced as follows. Here, formula (1) is the reaction that occurs when cured epoxy resin is cured with general amine, and formula (2) is the reaction that might have happened during solidification of coatings modified with nano-sized titanium powder.

From the equations, it can be seen that the titanium atom replaces the hydrogen atom of amidocyanogen and bonds with the active oxygen atom obtained by ring opening of epoxy group in the process of solidification. The reason is that with high surface energy, nano-sized powder titanium atoms are inclined to bond with the film forming matter around them to make the surface energy lower. In addition, as the II subgroup element, titanium atoms easily bond with oxygen atoms with electrons at p atomic orbital and with unfilled 3d energy band. So there is a p-d conjugative effect in the large molecular structure. Therefore, the bond energy is high. Many epoxy groups in epoxy resin are opened during the curing providing enough active oxygen atoms with electrons in p orbit to form p-d conjugative effect. As a result, bonding formed between additive and film former matter.⁸

Equation (3) can be obtained through Eq. (2) - Eq.(1).

From a thermodynamic perspective, as the bond energy of Ti–O and H–O is 661.9 kJ mol⁻¹, 428.0 kJ mol⁻¹, respectively, it could be concluded that the enthalpy of reaction (3), $\Delta_r H_3$, is approximately –185 kJ mol⁻¹, which is negative. According to references,⁹ when two high randomness substances are mixed, the mixed entropy change is very small, almost zero. Therefore, the Gibbs reaction energy of reaction (3) $\Delta_r G_3$, at room temperature is below zero. Owing to the relationships among $\Delta_r G_1$, $\Delta_r G_2$, and $\Delta_r G_3$ shown as Eq. (4) and Eq. (5) will be obtained.

$$\Delta_{\rm r}G_2 - \Delta_{\rm r}G_1 = \Delta_{\rm r}G_3 \tag{4}$$

$$\Delta_{\rm r}G_2 = \Delta_{\rm r}G_3 + \Delta_{\rm r}G_1 \tag{5}$$

Here, $\Delta_r G_3 < 0$, $\Delta_r G_1 < 0$.

$$\Delta_{\rm r}G_2 < 0. \tag{6}$$



So,

Therefore, it could be concluded that reaction (2) could have taken place during the curing of the coating. Thus, the nano-sized titanium powder added to the coating no longer exists in the form of a full machinery mixture. Due to the chemical key, a tight barrier layer is formed to prevent corrosive media such as water and oxygen from diffusing into the internal layer, which delays corrosion of the metal matrix. Moreover, thanks to the chemical key, the variation law for the resistance of the coating versus the increasing content of nano-sized titanium powder is different from that of coatings modified with 200 meshes titanium powder. In addition, due to this chemical bond, the toughness of the coating is not significantly different from lacquer coating.

Conclusions

Nano-titanium particles may be involved in the curing reaction of coatings. Therefore, the addition of titanium nano-sized powder did not significantly alter the physical properties of the coatings (toughness), and coatings modified with nano-sized titanium powder had better protection performance than the coatings with micrometre-sized titanium powder. Due to the chemical key between nano-sized titanium particles and the coating agent, the increase in the number of charge carriers in the coating due to the existence of the titanium metal is lower. For this reason, the resistance change order is different from the change law of the coating modified with the micrometre-sized titanium powder, and the change rule of the electrical resistance for the coatings modified with nano-sized titanium particles cannot be explained by the change of dielectric constants.

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List of symbols and abbreviations Popis simbola i kratica

- $\Delta_r G$ Gibbs energy of reaction, kJ mol⁻¹ – Gibbsova reakcijska energija, kJ mol⁻¹
- $\Delta_r H$ enthalpy of reaction, kJ mol⁻¹ – reakcijska entalpija, kJ mol⁻¹

- w mass fraction, % – maseni udjel, %
- CPS counts per second – broj registriranih signala u sekundi
- EIS electrochemical impedance spectroscopy – elektrokemijska impedancijska spektroskopija
- IR infrared spectroscopy – infracrvena spektroskopija
- XPS X-ray photoelectron spectroscopy – rendgenska fotoelektronska spektroskopija

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SAŽETAK

Utjecaj titanijevih nanočestica na antikorozivna svojstva epoksidnih lakova na čeliku

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Proučavana su zaštitna svojstva epoksidnih asfaltnih premaza s masenim udjelima titanijeva praha 2 %, 5 %, 10 % i 20 % te nanočestica titanija u masenim udjelima 0 %, 5 %, 10 % i 20 % elektrokemijskom impedancijskom spektroskopijom (EIS) i raspršivanjem soli. Strukture premaza proučavane su infracrvenom spektroskopijom i rendgenskom fotoelektronskom spektroskopijom (XPS).

Rezultati pokazuju da bi nanometarske čestice titanija mogle sudjelovati u učvršćivanju laka. Dodatak nanočestica titanija ne mijenja značajno fizička svojstva laka (žilavost). Lakovi s nanočesticama titanija bolje štite od lakova s mikrometarskim titanijevim prahom. Istodobno, zbog kemijskog međudjelovanja nanočestica titanija i laka, slabije je izraženo povećanje broja nosilaca naboja. Stoga ovisnost svojstava lakova o količini titanija nije jednaka u slučaju mikrometarskih ili nanometarskih čestica. Promjena električne otpornosti lakova modificiranih nanočesticama titanija ne može se objasniti promjenom dielektrične konstante.

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